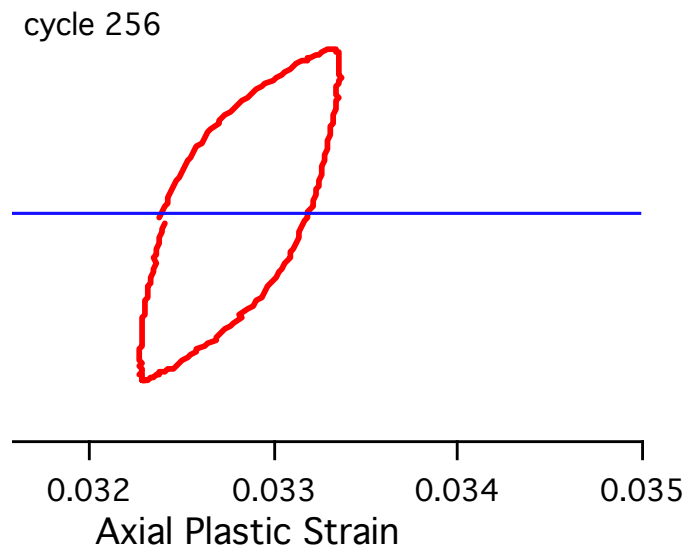
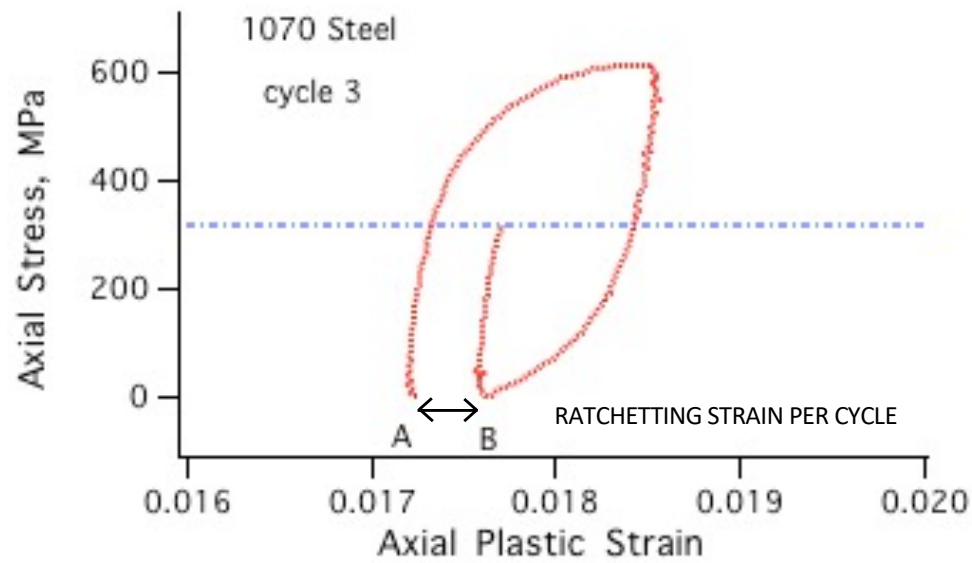


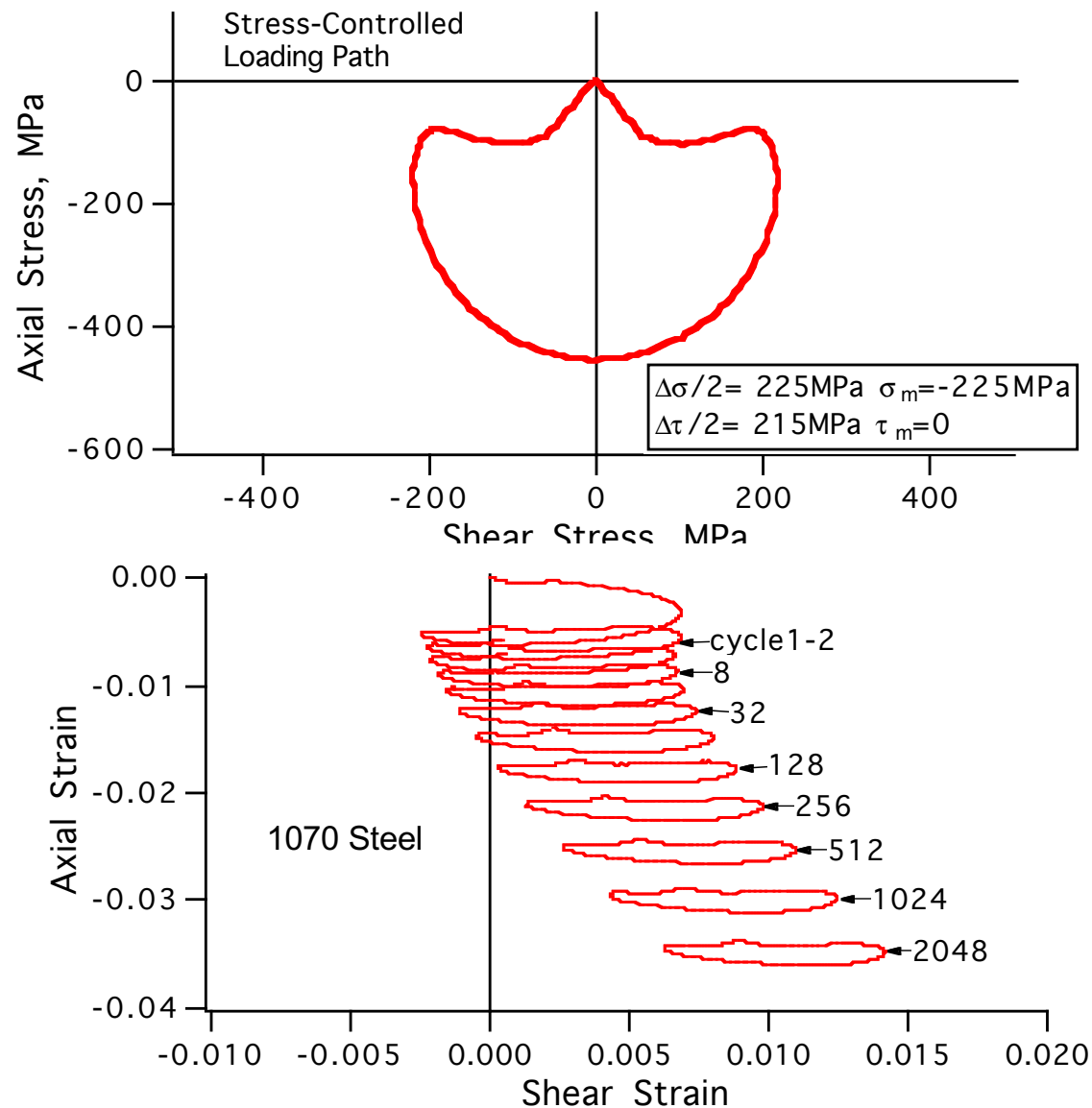
# DEFINITION OF RATCHETTING : INCREMENT OF STRAIN PER CYCLE DUE NONCLOSURE OF THE HYSTERESIS LOOP



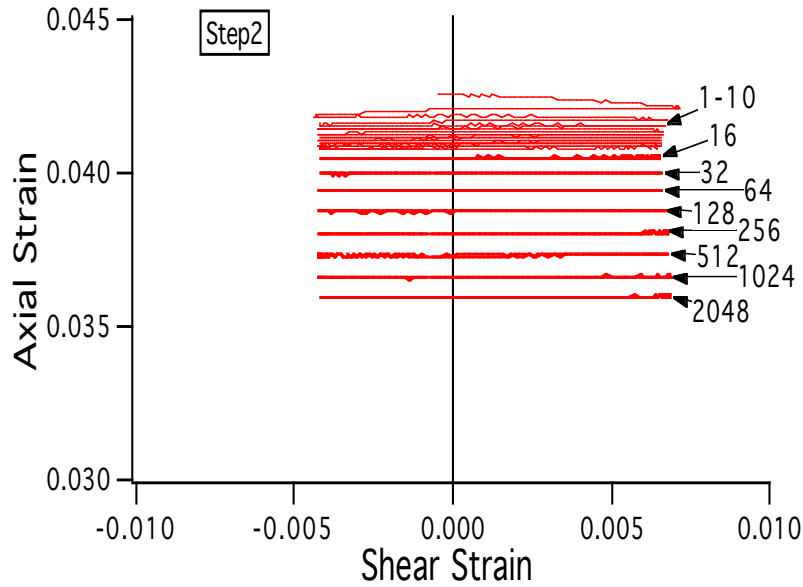
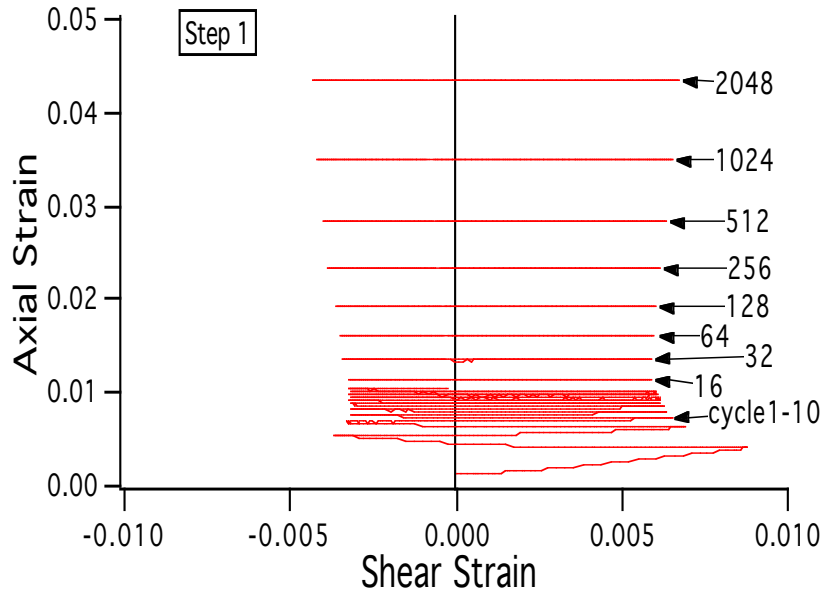
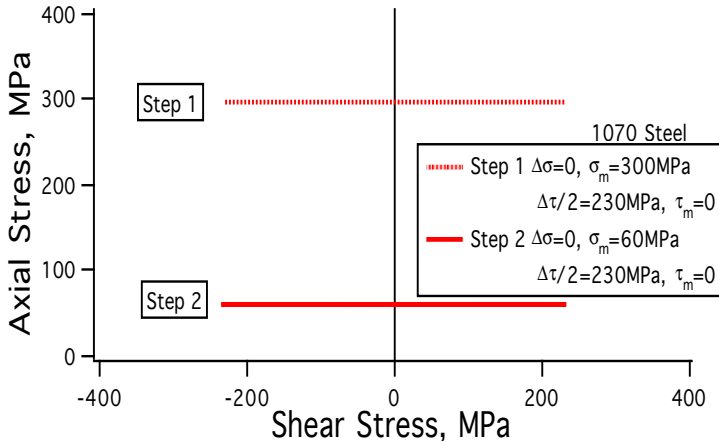
# EXPERIMENTAL RATCHETTING FOR A NOPROPORTIONAL AXIAL-TORSIONAL LOADING PATH

Jiang, Y. and H. Sehitoglu, *ASME JAM*, 63, 726-733, 1996.

Jiang, Y. and H. Sehitoglu, *ASME JAM*, 63, 720-725, 1996.



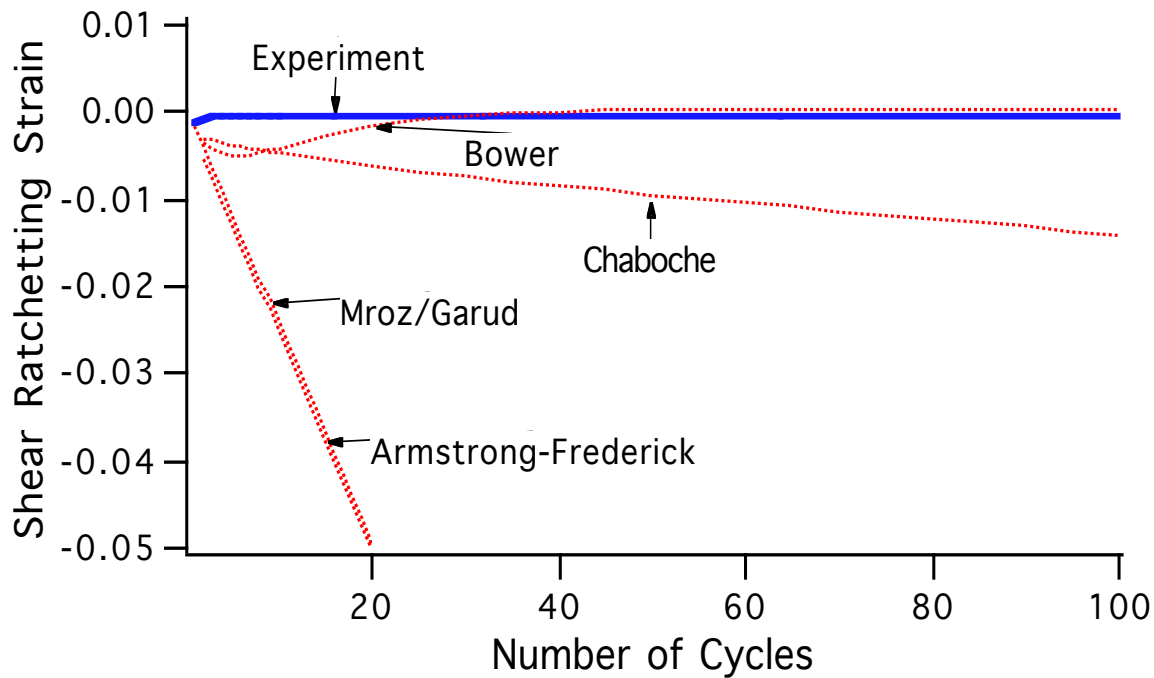
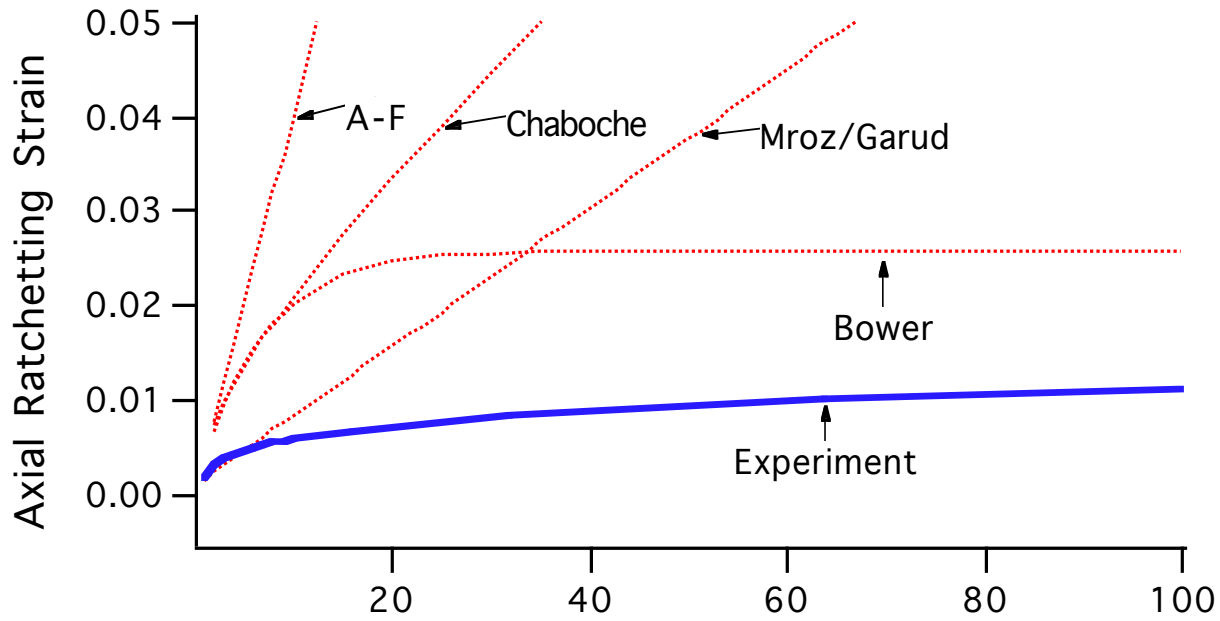
# EXPERIMENTAL RATCHETTING FOR A TWO-STEP NONPROPORTIONAL LOADING HISTORY



# EXPERIMENTAL OBSERVATIONS

- The ratchetting direction is coincident with the mean stress direction under single-step proportional loading.
- For 1070 Steel, the ratchetting rate decreases with increasing number of loading cycles for both proportional and nonproportional loadings.
- Under multiple-step loadings, the material exhibits a memory of the previous loading history.

# PREDICTION OF THE "ELLIPSE" PATH



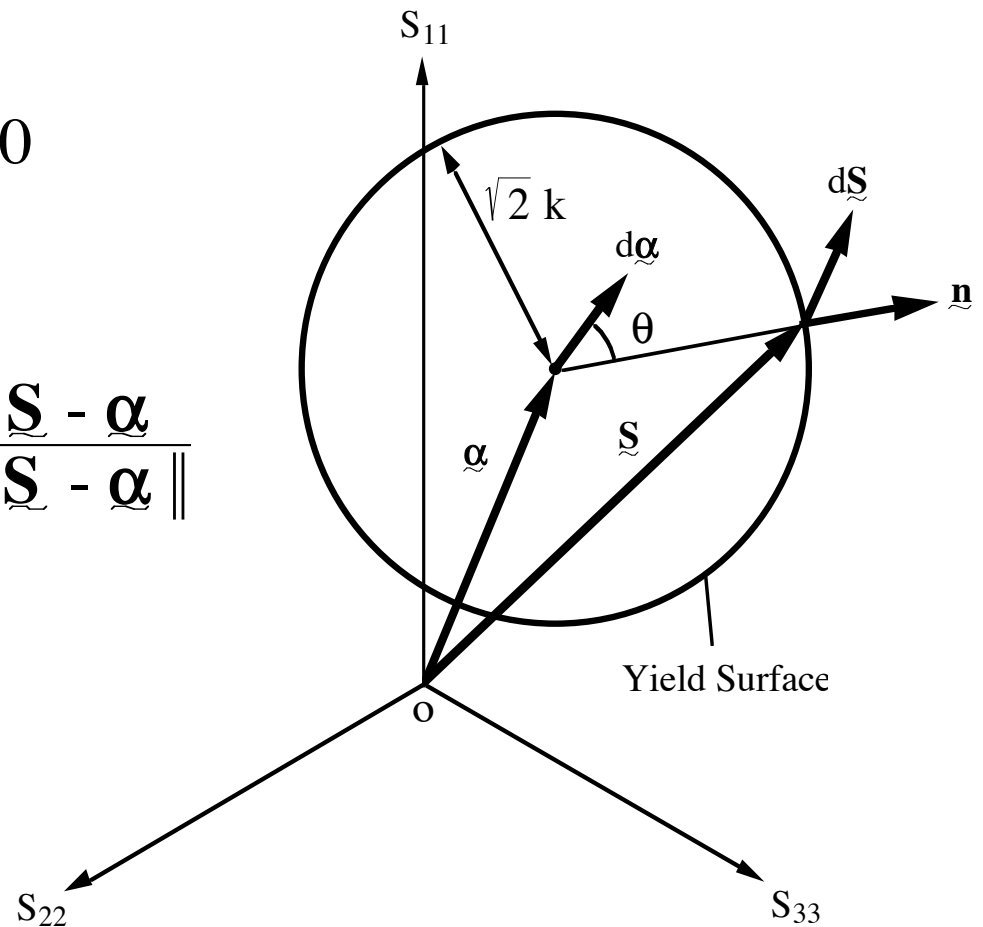
# Plasticity Fundamentals

$$f = (\underline{\mathbf{S}} - \underline{\boldsymbol{\alpha}}) : (\underline{\mathbf{S}} - \underline{\boldsymbol{\alpha}}) - 2k^2 = 0$$

$$d\underline{\boldsymbol{\epsilon}}^p = \frac{1}{h} \langle d\underline{\mathbf{S}} : \underline{\mathbf{n}} \rangle \underline{\mathbf{n}} \quad \underline{\mathbf{n}} = \frac{\underline{\mathbf{S}} - \underline{\boldsymbol{\alpha}}}{\| \underline{\mathbf{S}} - \underline{\boldsymbol{\alpha}} \|}$$

$$df = 0$$

$$d\underline{\mathbf{S}} : \underline{\mathbf{n}} - d\underline{\boldsymbol{\alpha}} : \underline{\mathbf{n}} - 2k \, dk = 0$$



## EVOLUTION OF BACK STRESS

$$d\boldsymbol{\alpha}^{(i)} = f_1^{(i)} (\underline{\mathbf{n}} - f_2^{(i)} \underline{\mathbf{L}}^{(i)}) dp \quad (i=1, 2, \dots, M)$$

$$M=1 \quad f_1^{(1)} = a_a \quad f_2^{(1)} = \frac{c_a}{a_a} \|\boldsymbol{\alpha}\|$$

$$f_1^{(i)} = c^{(i)} r^{(i)} \quad f_2^{(i)} = \frac{\|\boldsymbol{\alpha}^{(i)}\|}{r^{(i)}} \quad (i=1, 2, \dots, M)$$

$$f_1^{(i)} = c^{(i)} r^{(i)} \quad f_2^{(i)} = \left( \frac{\|\boldsymbol{\alpha}^{(i)}\|}{r^{(i)}} \right)^{\chi^{(i)+1}} \langle \underline{\mathbf{n}} : \underline{\mathbf{L}}^{(i)} \rangle$$

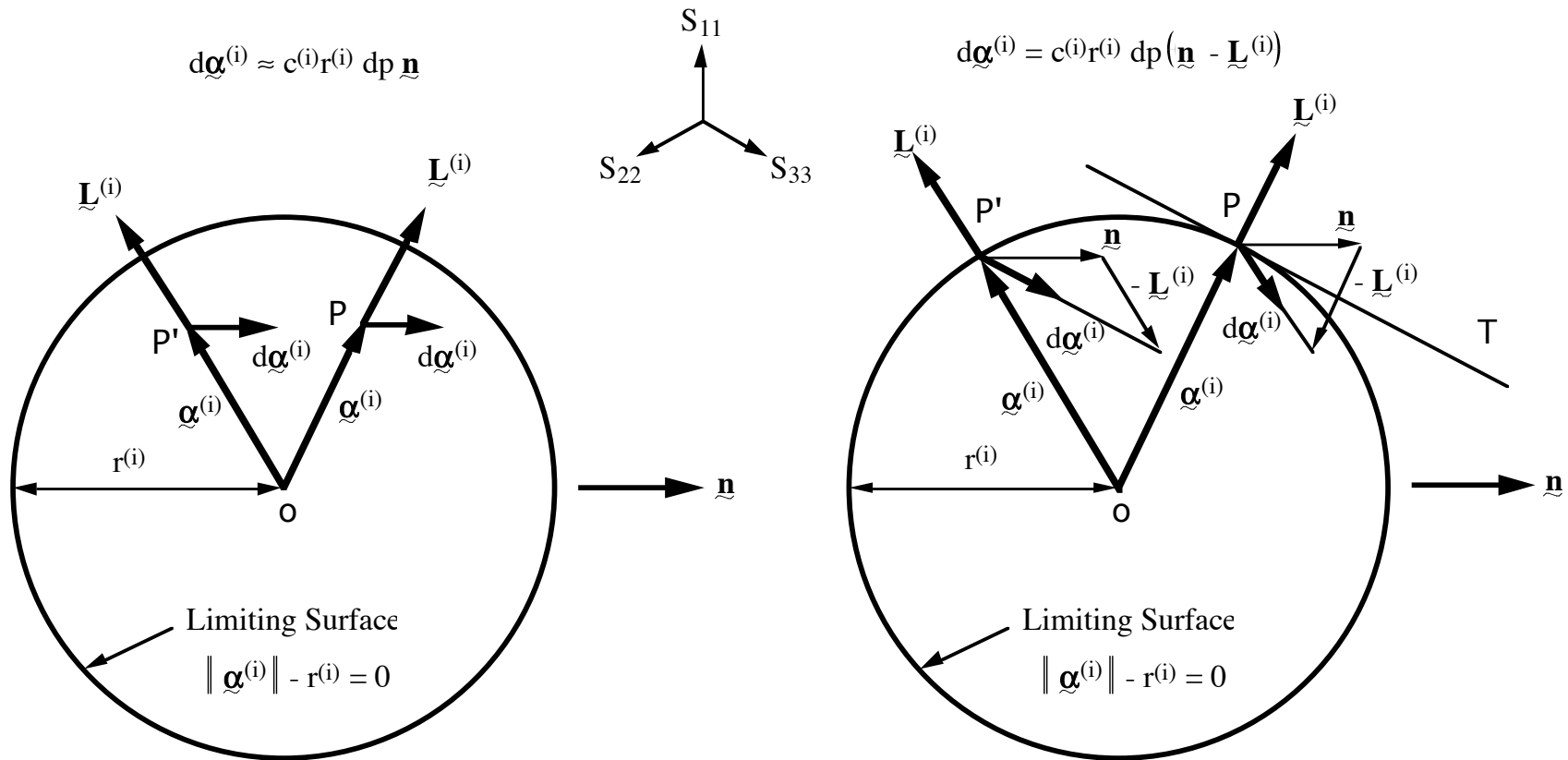
(i=1, 2, ..., M)

# NEW PLASTICITY MODEL

Jiang, Y. and H. Sehitoglu, *ASME JAM*, 63, 726-733, 1996.

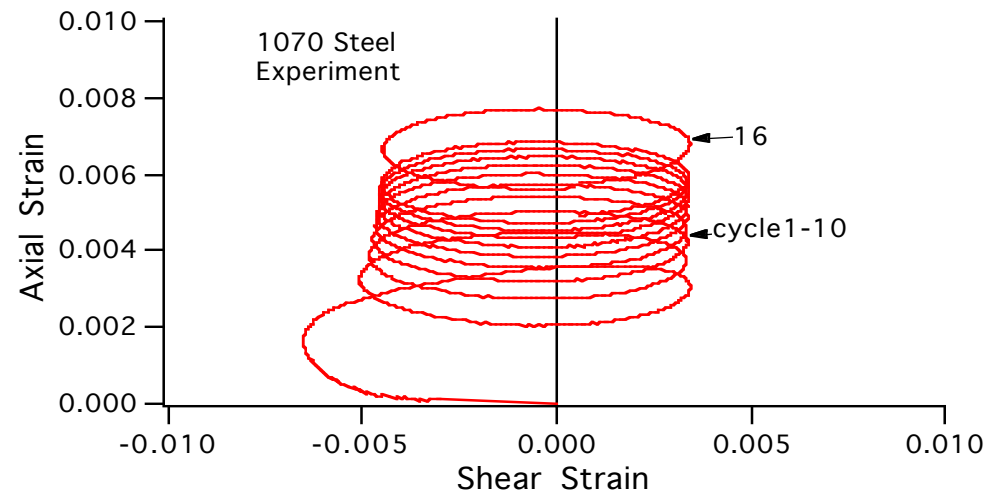
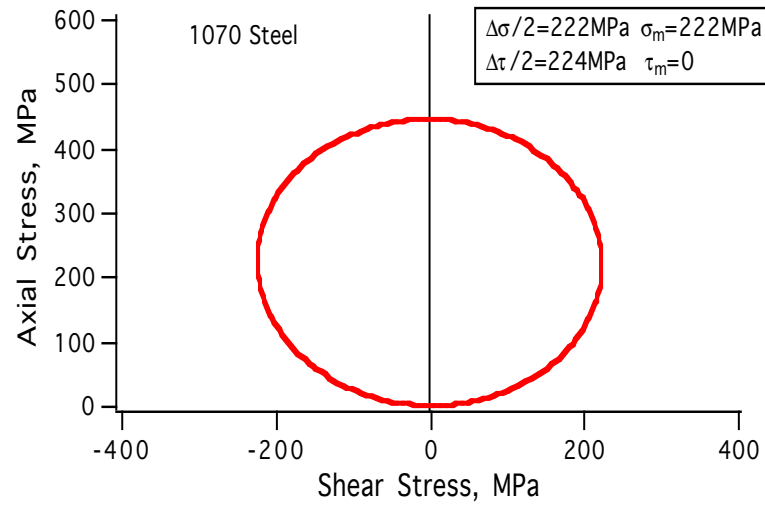
Jiang, Y. and H. Sehitoglu, *ASME JAM*, 63, 720-725, 1996.

$$\underline{\alpha} = \sum_{i=1}^M \underline{\alpha}^{(i)} \quad d\underline{\alpha}^{(i)} = c^{(i)} r^{(i)} \left( \underline{n} - \left( \frac{\|\underline{\alpha}^{(i)}\|}{r^{(i)}} \right) \chi^{(i)+1} \underline{L}^{(i)} \right) dp \quad (i=1, 2, \dots, M)$$

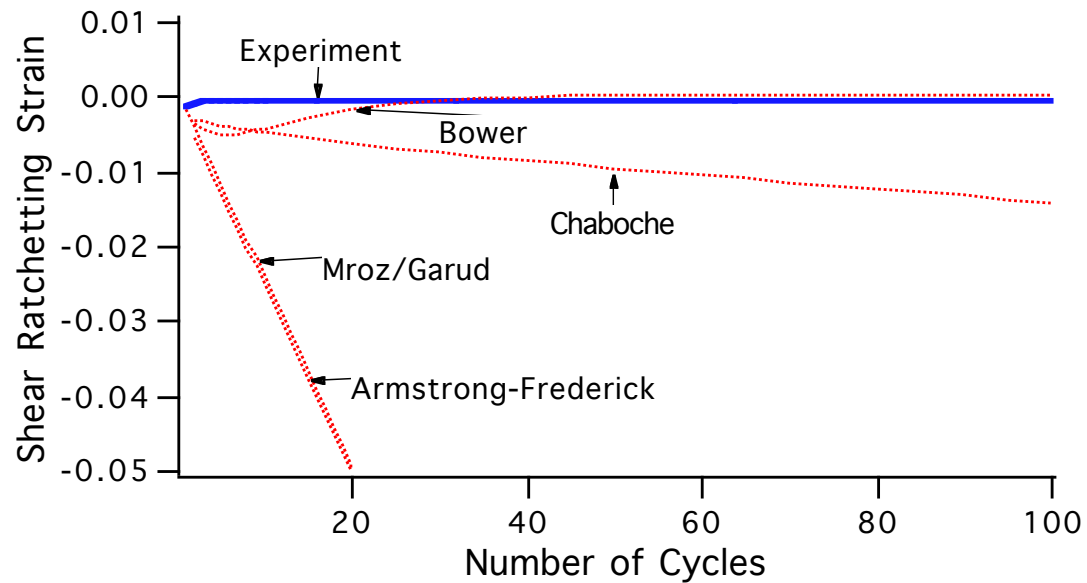
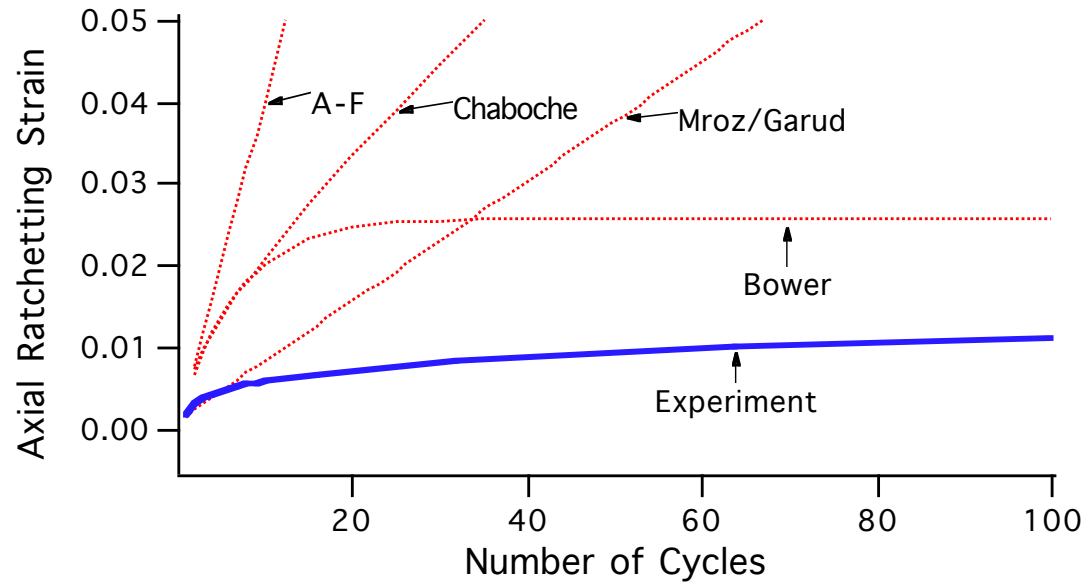




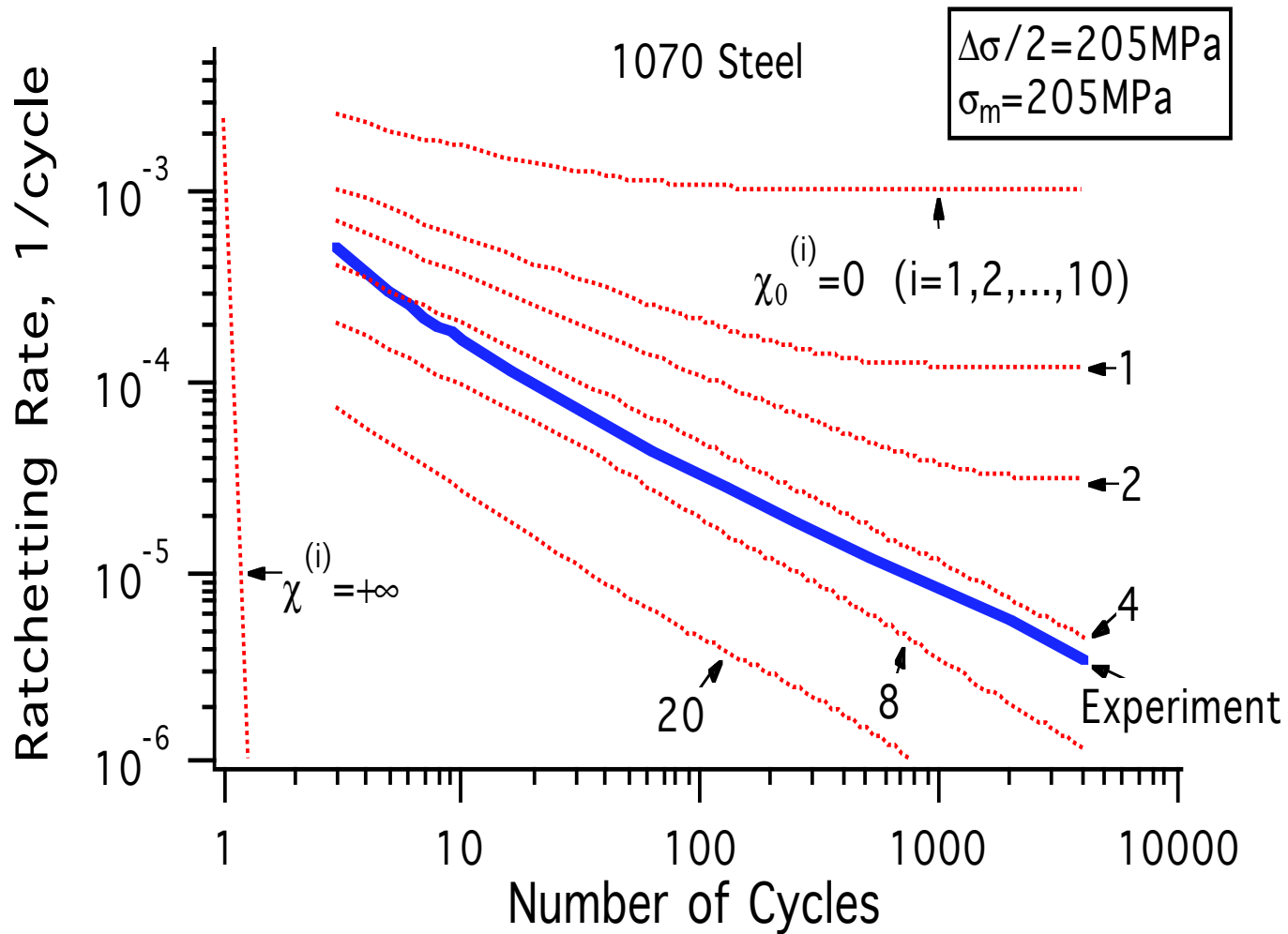
# EXPERIMENTAL “ELLIPSE PATH”



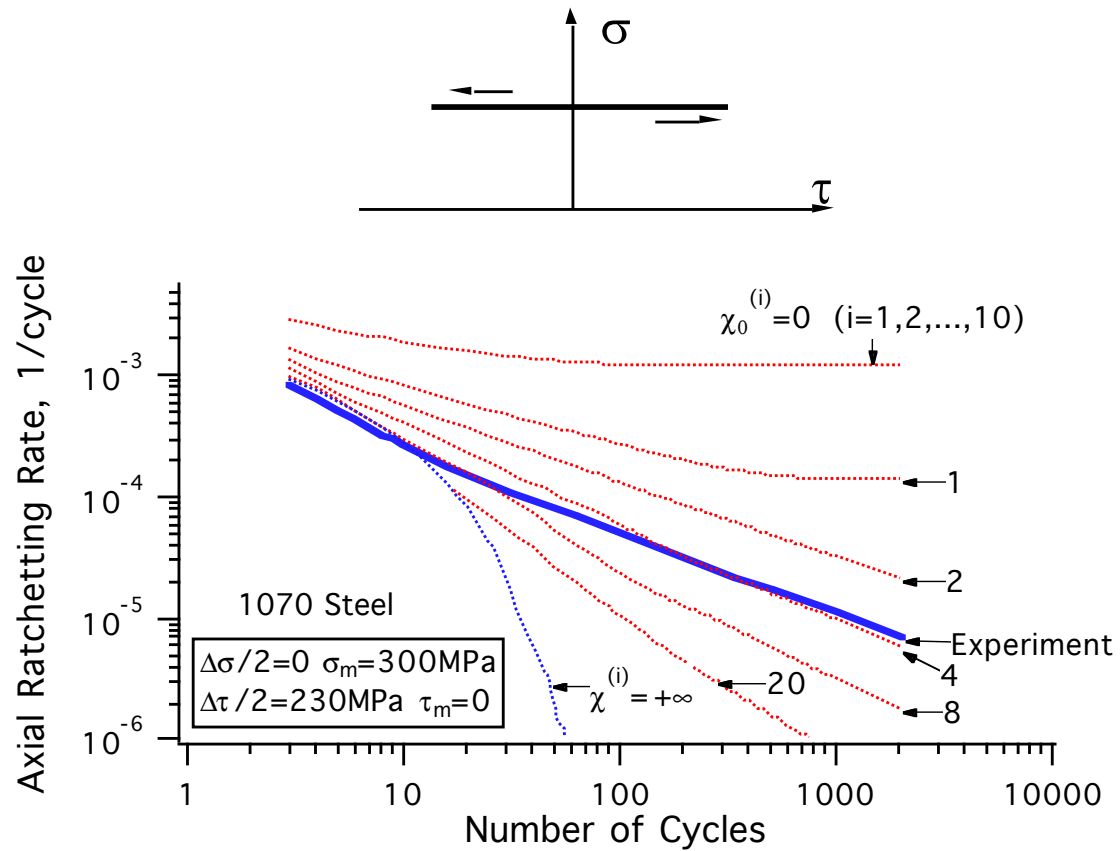
# PREDICTION OF THE "ELLIPSE" PATH



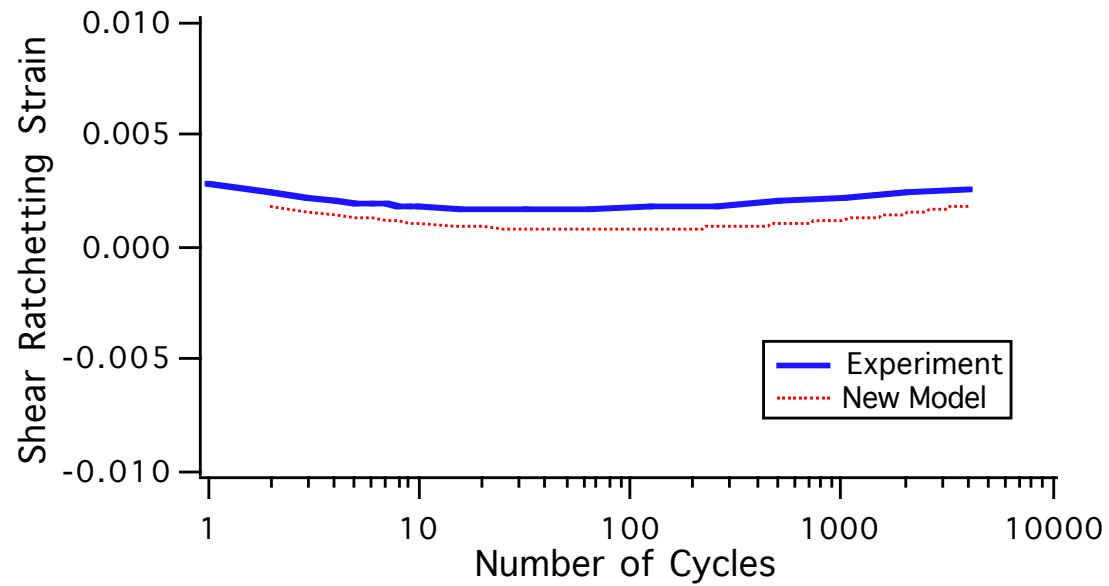
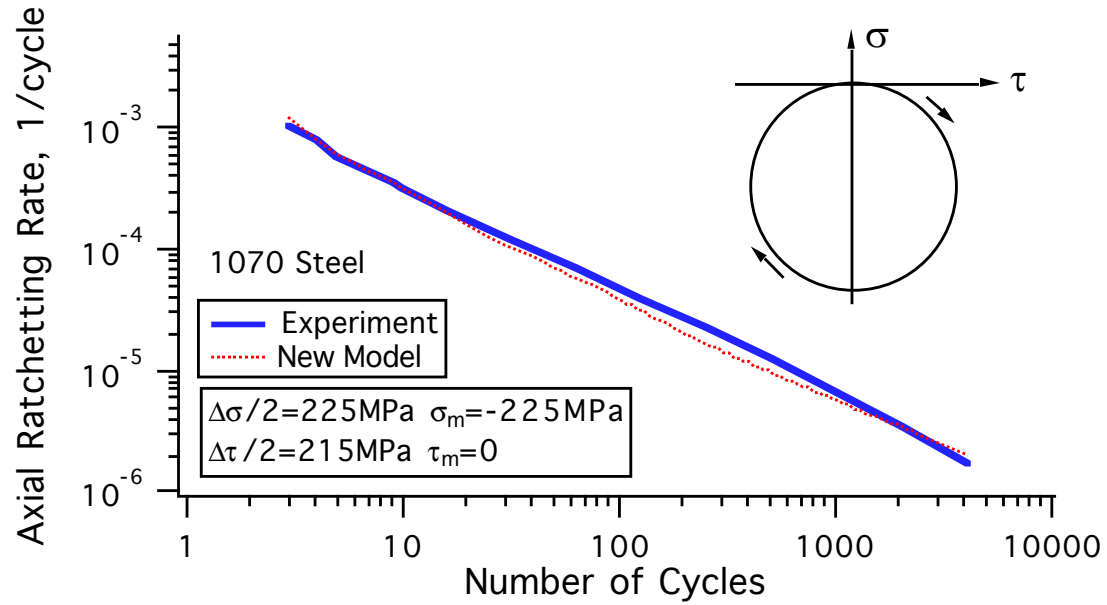
# CAPABILITY OF PROPOSED MODEL IN UNIAXIAL LOADING



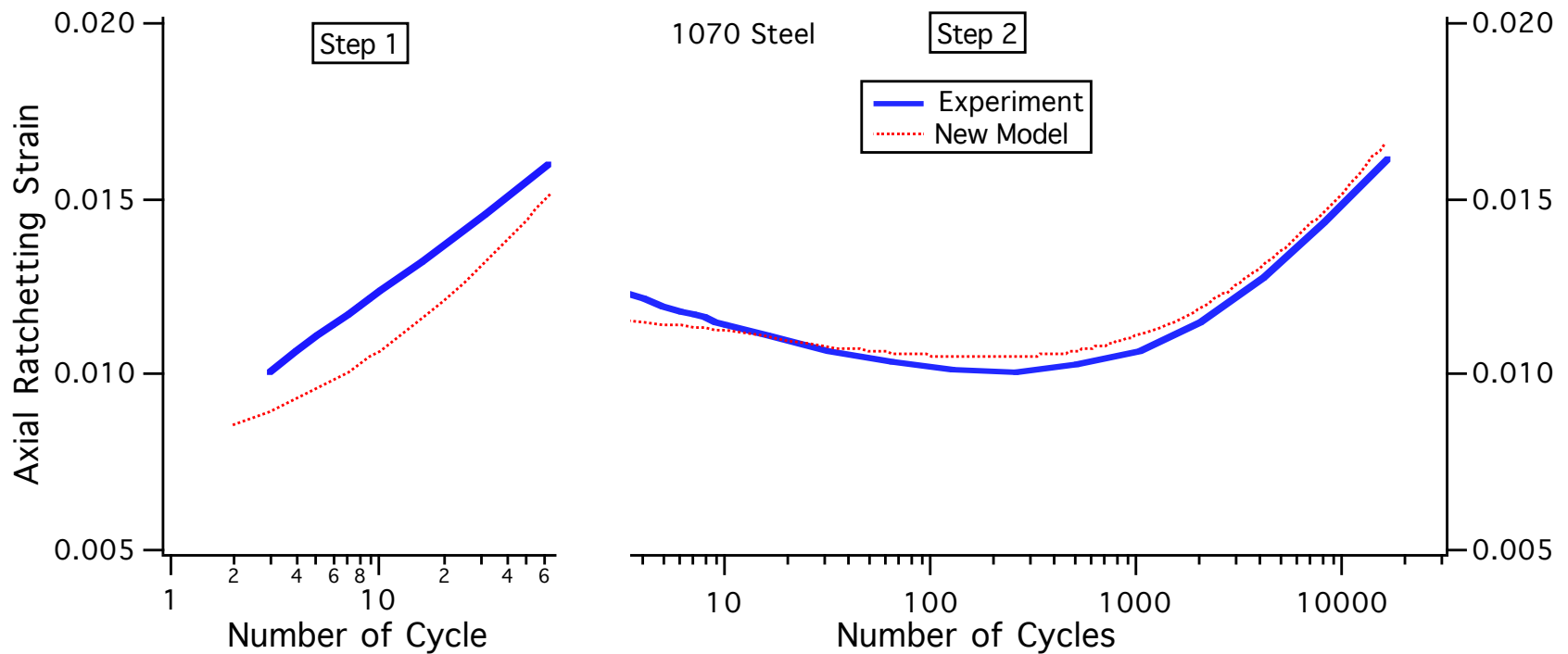
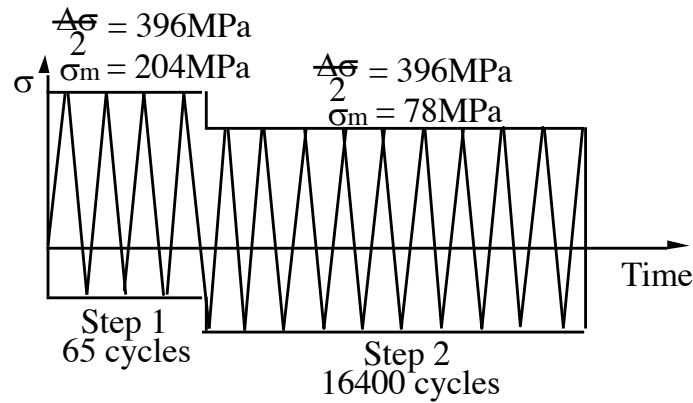
# CAPABILITY OF PROPOSED MODEL IN NONPROPORTIONAL LOADING



# CAPABILITY OF PROPOSED MODEL IN NONPROPORTIONAL LOADING



# PREDICTION OF RATCHETTING RATES IN TWO STEP PROPORTIONAL LOADING



# Jiang-Sehitoglu (JS) Plasticity Model

- Only model that can predict ratcheting under complex loading scenarios
- Backstress is divided into multiple components
- Translation of the backstress is not constricted to the direction of the normal
- Elastic stress state is computed first, and a relaxation procedure is implemented to determine the final stress state

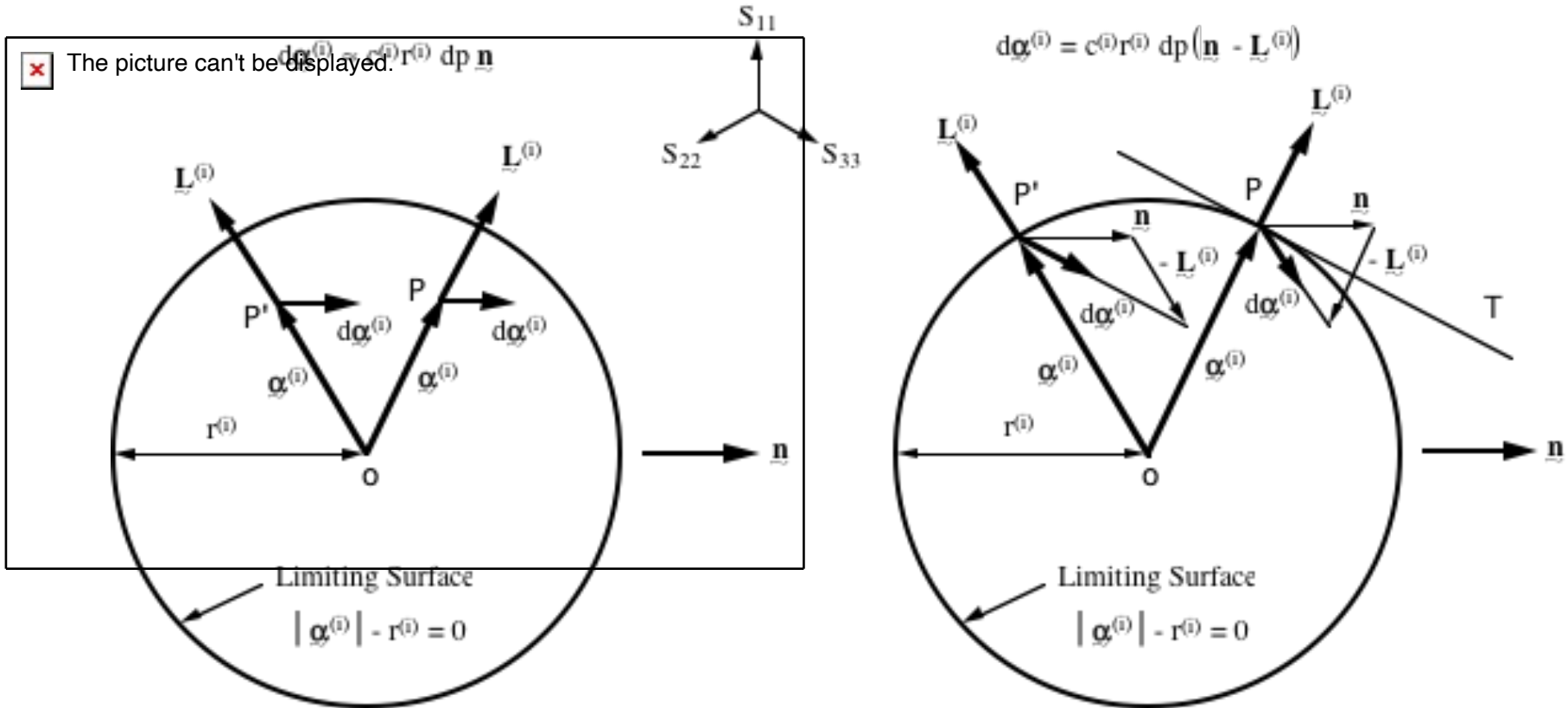
# JS Plasticity Model

Jiang, Y. and H. Sehitoglu, *ASME JAM*, 63, 726-733, 1996.

Jiang, Y. and H. Sehitoglu, *ASME JAM*, 63, 720-725, 1996.

3 Constant Sets Are Needed

$$\underline{\alpha} = \sum_{i=1}^M \underline{\alpha}^{(i)} \quad d\underline{\alpha}^{(i)} = c^{(i)} r^{(i)} \left( \underline{n} - \left( \frac{\|\underline{\alpha}^{(i)}\|}{r^{(i)}} \right) \chi^{(i)+1} \underline{L}^{(i)} \right) dp \quad (i=1, 2, \dots, M)$$

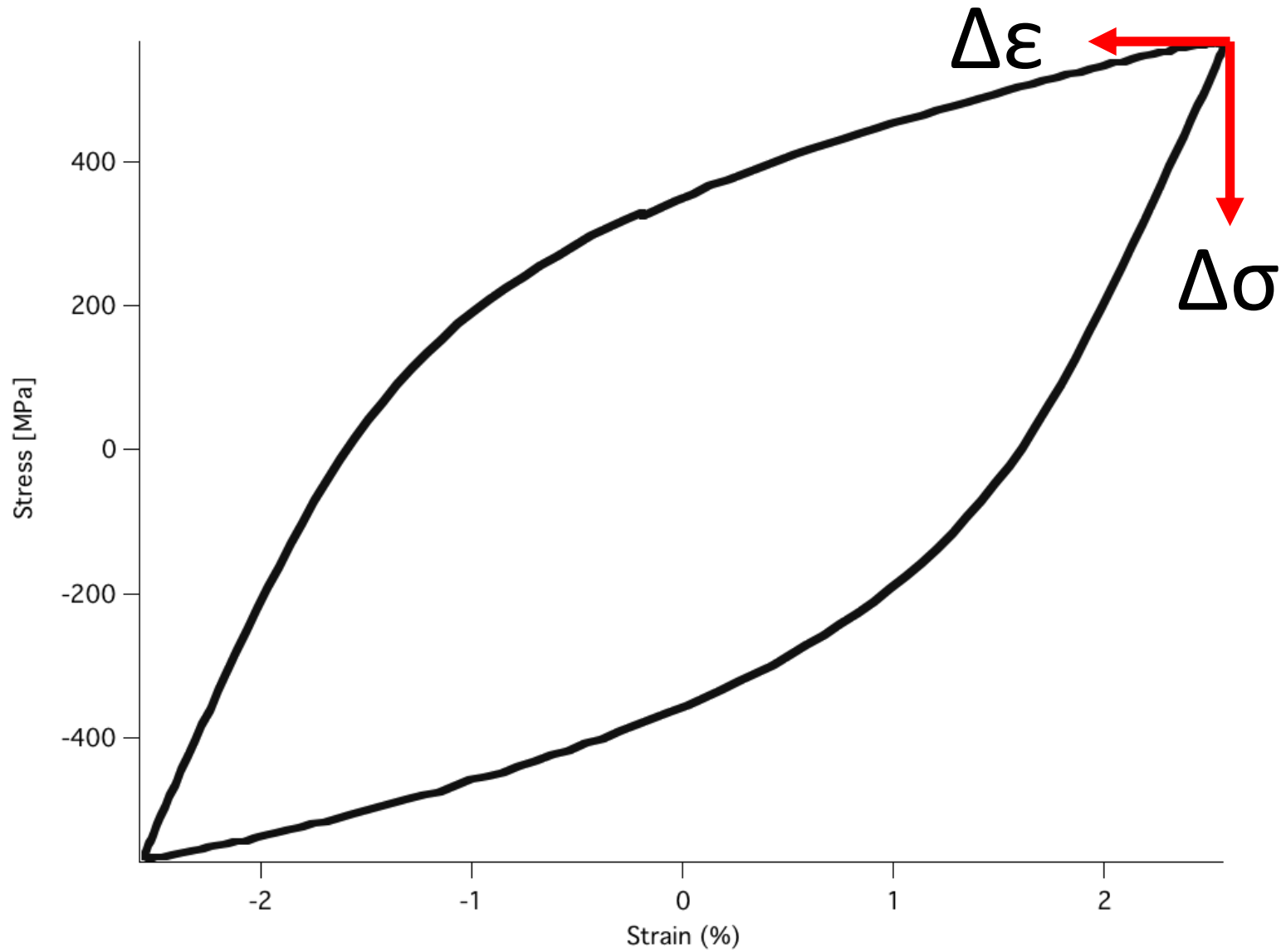




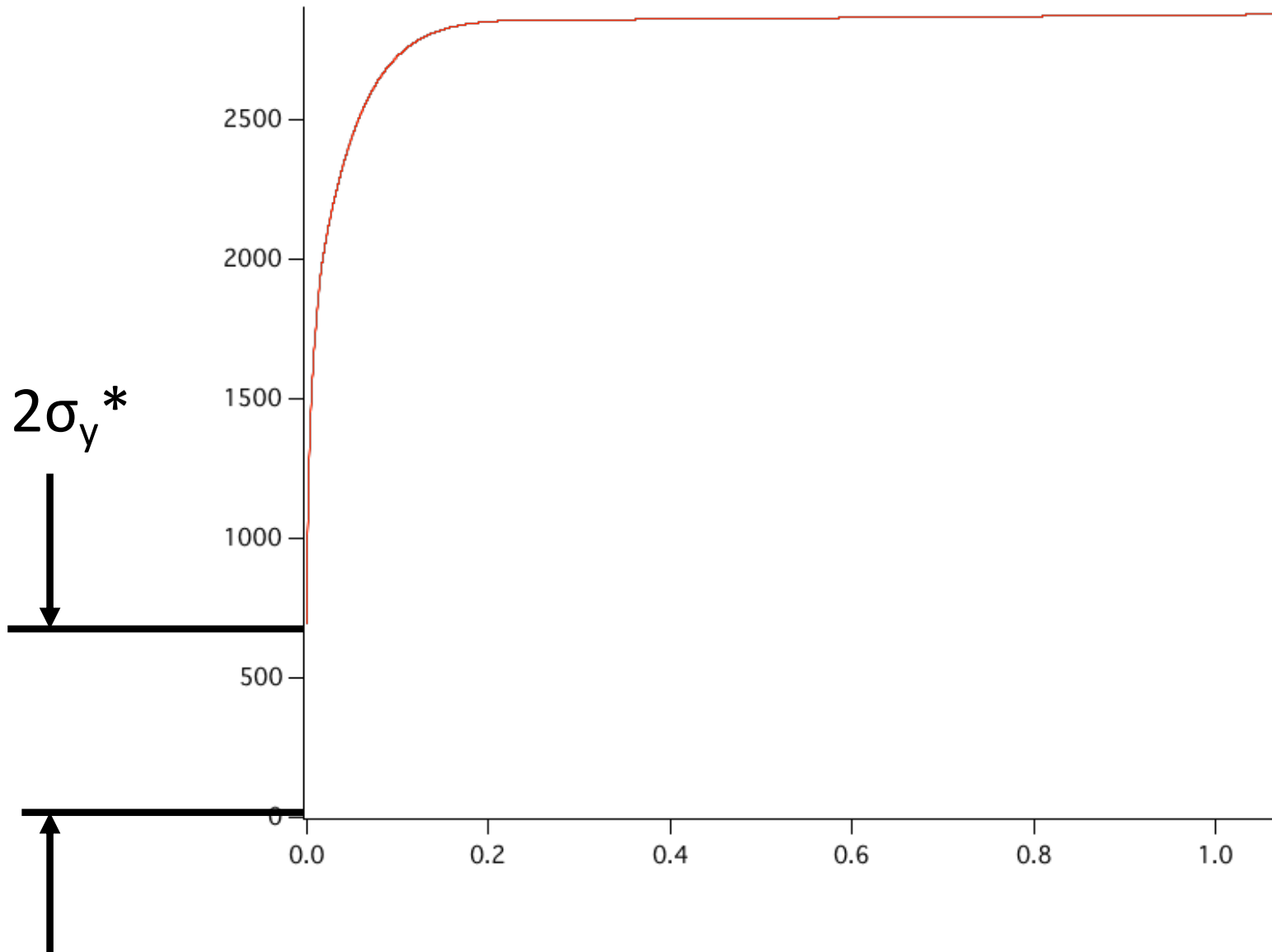
# Material Constant Sets

- $r^{(i)}$  and  $c^{(i)}$ 
  - Define the stress-strain behavior of the material in a linear piece-wise manner
  - Determined from fully reversed stress-plastic strain data
- $\chi^{(i)}$ 
  - Defines the ratcheting rate decay of the material
  - Determined from uniaxial ratcheting experiments

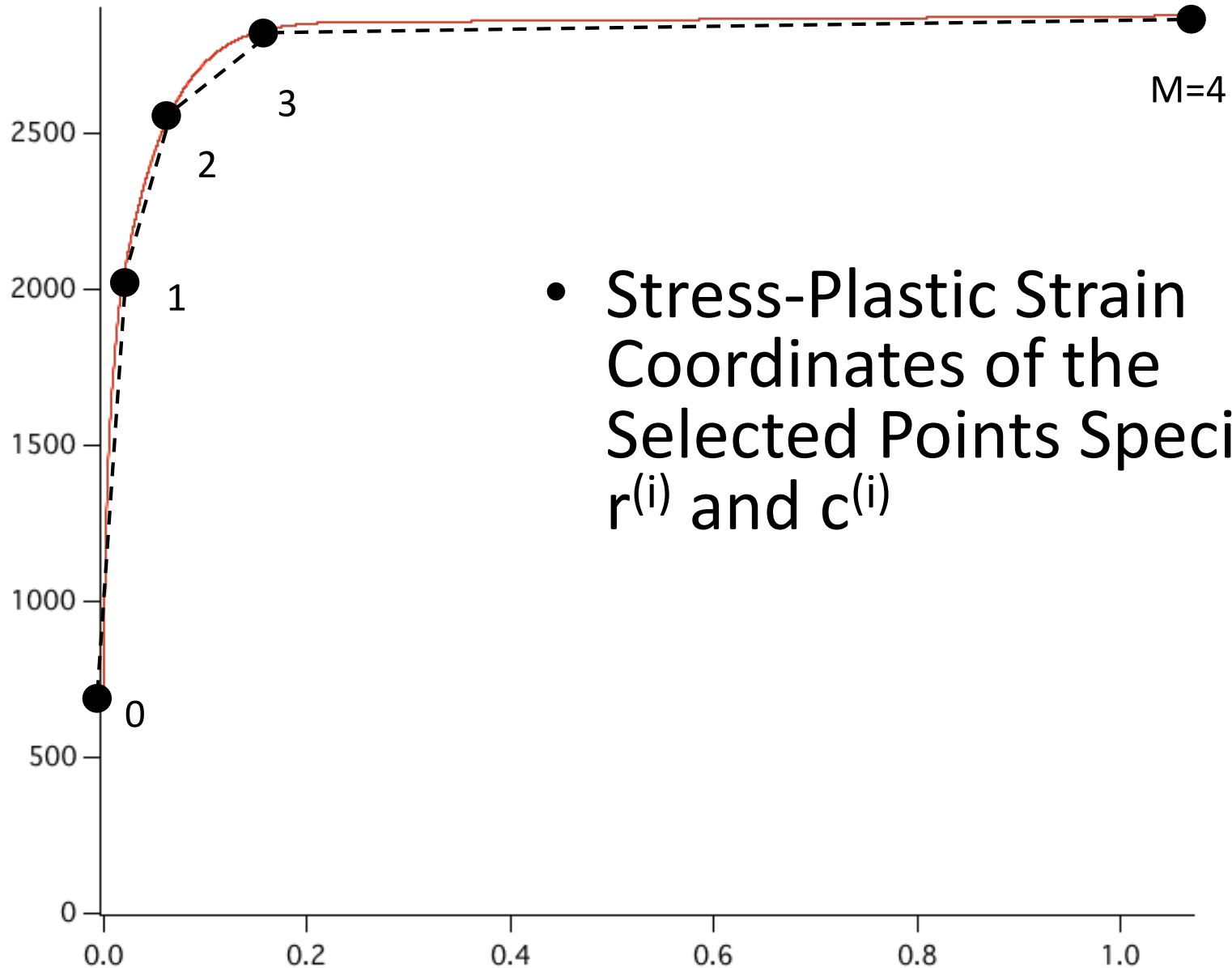
# Pearlite Stress-Strain Data



# Eliminate the Elastic Strain



# Select Piece-Wise Linear Segments



- Stress-Plastic Strain Coordinates of the Selected Points Specify  $r^{(i)}$  and  $c^{(i)}$

# Determining $X$

- Plot uniaxial ratcheting rate from experimental data
- Simulate ratcheting rate from JS model
  - Use  $r^{(i)}$  and  $c^{(i)}$  determined above
  - Guess a value for  $X$
- Trial and Error until the simulated curve equals the experimental curve